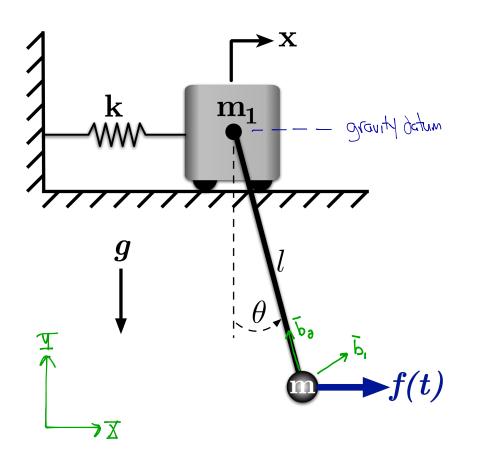
Example



2 bodies, 2 DOF -> 2 generalized cours and 2 Eq of

Ux opereralised coach (x, b)

The velocity of m, is x

Q: What is the velocity of m?

It depends on both X and O

$$\overline{U}_{0} = \dot{\chi} \overline{I} + 10 \overline{D}_{0} \leftarrow \overline{D}_{0} = \cos 0 \overline{I} + \sin 0 \overline{J}$$

$$= (\dot{\chi} + \dot{J} \dot{\Theta} \cos 0) \overline{I} + (\dot{J} \dot{\Theta} \sin 0) \overline{J}$$

a What should we choose as the growity datum? Let's choose the attedment point (The back chooses the "lowest" pendulum paint)

Now, form the energies, then the Lockardian

 $T = \frac{1}{2}m_{1}\dot{\chi}^{2} + \frac{1}{2}m_{0}\ddot{\eta}^{2} = \frac{1}{2}m_{0}\dot{\chi}^{2} + \frac{1}{2}m\left[\left(\dot{\chi} + 10\cos\theta\right)\bar{I} + \left(10\sin\theta\right)\bar{J}\right] \cdot \left[\left(\dot{\chi} + 10\cos\theta\right)\bar{I} + \left(10\sin\theta\right)\bar{J}\right]$ (or 3 m \(\bar{\sqrt{1}}\)

 $T = \frac{1}{2}m_1X^2 + \frac{1}{2}m\left[\left(x + 10\cos\theta\right)^2 + \left(10\sin\theta\right)^2\right] \leftarrow Total \quad \text{kinetic energy}$

V = VGr + VSD

 $\sqrt{gr} = mgh = -mglose$ and $\sqrt{sp} = \frac{1}{2}kx^2$

V = -mgloss + 1/2 x2 = Total potential energy

[= T-V ← Lograngion

Q What about the external force, f(+)? \ We have to find the Qi terms for Lagrange's Eq To do so, we'll use victal displacements and without work We know that $V_2 = (x + 10 \cos\theta) \overline{1} + (10 \sin\theta) \overline{5} \leftarrow \text{use this volacity to figure out the virtual}$ displaments. $\frac{d\overline{c}}{dt} = \left(\frac{dx}{dt} + \sqrt{\frac{d\theta}{t}}\cos dt\right) + \left(\sqrt{\frac{d\theta}{t}}\sin \theta\right) = \frac{1}{2}\left(\frac{d\theta}{t}\cos \theta\right) + \frac{1}{2}\left(\frac{d\theta}{t}\cos \theta\right) + \frac{1}{2}\left(\frac{d\theta}{t}\cos \theta\right) = \frac{1}{2}\left(\frac{d\theta}{t}\cos \theta\right) + \frac{1}{2}\left(\frac{d\theta}{t}\cos \theta\right) + \frac{1}{2}\left(\frac{d\theta}{t}\cos \theta\right) = \frac{1}{2}\left(\frac{d\theta}{t}\cos \theta\right) + \frac{1}{2}\left(\frac{d\theta}{t}\cos \theta\right) = \frac{1}{2}\left(\frac{d\theta}{t}\cos \theta\right) + \frac{1}{2}\left(\frac{d\theta}{t}\cos \theta\right) +$ $\int_{\overline{r}_2} = (\int_X + | \int_{\overline{r}_2} \cos \theta) \overline{1} + (| \int_{\overline{r}_2} \sin \theta) \overline{2} \leftarrow \text{virtual displacement of } m$

Example (cont.)

To find
$$Q_i$$
, we need to find the virthal work date by the force (= Force · Virthal displacement)
$$IW = f \vec{I} \cdot d\vec{r}_{0} = f \vec{I} \cdot \left[(dx + 1d\theta \cos \theta) \vec{I} + (d\theta \sin \theta) \vec{J} \right] = F(dx + 1d\theta \cos \theta)$$

$$IW = F dx + (Fl \cos \theta) d\theta$$

$$Q_{0} dq_{0}$$

$$IW = Q_{0} dq_{0}$$

$$\frac{\partial_{1} = \chi}{\partial t} = \frac{\partial}{\partial x} - \frac{\partial}{\partial x} = 0$$

$$\frac{\partial}{\partial x} = m_{1}x + \frac{1}{2}m \left[\frac{\partial}{\partial x} (x + 10\cos\theta) \right] \qquad \frac{\partial}{\partial x} = -kx$$

$$\frac{\partial}{\partial t} \left(\frac{\partial L}{\partial x} \right) = m_{1}x + m \left(x + 10\cos\theta - 10^{2}\sin\theta \right) \qquad \frac{\partial}{\partial x} = -kx$$

$$\frac{\partial}{\partial t} \left(\frac{\partial L}{\partial x} \right) = m_{1}x + m \left(x + 10\cos\theta - 10^{2}\sin\theta \right) \qquad \frac{\partial}{\partial x} = -kx$$

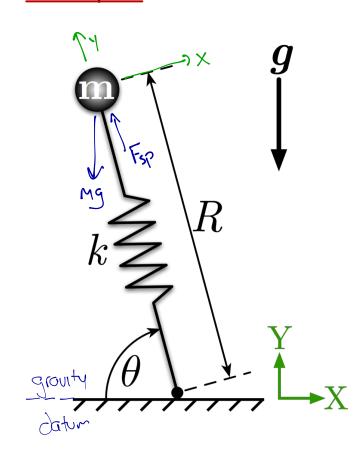
$$\frac{\partial}{\partial x} \left(\frac{\partial L}{\partial x} \right) = m_{1}x + m \left(x + 10\cos\theta - 10^{2}\sin\theta \right) \qquad \frac{\partial}{\partial x} = -kx$$

$$\frac{d}{dt}\left(\frac{\partial L}{\partial \theta}\right) - \frac{\partial L}{\partial \theta} = Q_{2}$$

$$\frac{d}{dt}\left(\frac{\partial L}{\partial \theta}\right) - \frac{d}{d\theta} = Q_{2}$$

$$= m \left[l_{x} cos \theta + l_{\theta} e^{-1} cos^{2} \theta + l_{\theta} e^{-1} cos^{2} \theta + l_{\theta} e^{-1} e^{1} e^{-1} e$$

Example



Spring Loaded Inverted Pendulum (SLIP) Model often used to model walking

Here, well assum were always in contact with the ground

This would be called

the stance phase

$$V = U_{grou} + U_{sp}$$

$$U_{grou} = M_{g}R SIn\Theta \qquad U_{p} = \frac{1}{3}K(R-L_{o})^{2}$$

$$V = M_{g}R SIn\Theta + \frac{1}{3}K(R-L_{o})^{2}$$

Now, write Lagrange's Equations for each gen. coord

$$\frac{\text{for } q = R}{\text{at} \left(\frac{\partial L}{\partial \dot{R}} \right) - \frac{\partial L}{\partial R} = 0}$$

$$\frac{2}{3\dot{R}} = m\dot{R}$$
 $\frac{d}{dt} \left(\frac{\partial L}{\partial \dot{R}}\right) = m\dot{R}$ $\frac{d}{\partial R} = 2m\dot{R}\dot{\theta} - mg\sin\theta + k(R-L_0)$

Example (cont.)

$$\frac{3}{4}\left(\frac{36}{36}\right) - \frac{36}{36} = 0$$

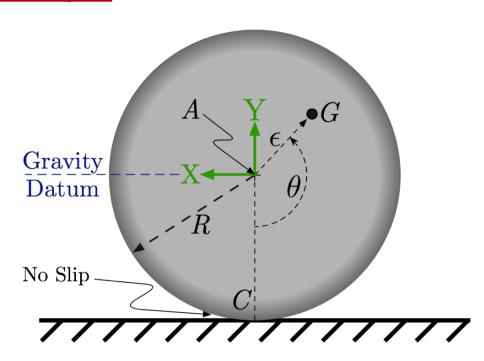
$$\frac{\partial L}{\partial \dot{G}} = MR^2 \dot{G}$$

$$\frac{\partial L}{\partial \dot{G}} = 2MRR\dot{G} + MR^2 \ddot{G}$$

Q: How would no hardle integrating the flight phose? (when feet/spring leaves the grand)

Generate a separate model for that phase. In simulation, we'd need to check for the spring going into extension at each step. At that transition, we'd switch to the flight model, using the system states at that transition as the initial conditions for the flight phase of simulation. During the flight phase of the simulation, we'd check for ground contact at each step of the solution. Once we see contact, we'd use the state at contact as the initial condition for the next stance phase. This process would repeat over the simulation duration.

Example



Want the equations of motion

$$\overline{V}_{A} = R\dot{\Theta}\overline{I}$$

$$\overline{V}_{G} = \overline{V}_{A} + \overline{\omega} \times \overline{C}_{OIA} \qquad \overline{\omega} = -\dot{\Theta}\overline{K}$$

$$= R\dot{\Theta}\overline{I} + (-\dot{\Theta}\overline{K} \times \varepsilon(-\sin\theta\overline{I} - \cos\Theta\overline{J}))$$

$$= R\dot{\Theta}\overline{I} + (\varepsilon\dot{\Theta}\sin\Theta\overline{J} - \varepsilon\dot{\Theta}\cos\Theta\overline{I})$$

$$\overline{V}_{G} = (R\dot{\Theta} - \varepsilon\dot{\Theta}\cos\Theta)\overline{I} + (\varepsilon\dot{\Theta}\sin\Theta)\overline{J}$$

For knetic energy, we need to consider both translation and votation T= 1/2 I DISK22 62 + 1 M VG·VG = 1/2 12 63, 1 M (RO-EDCOSE)2 + (ED SMO)2) $=\frac{1}{2}I_{22}\dot{\theta}^{2}+\frac{1}{2}m\left(R^{2}\dot{\theta}^{2}-2R\dot{\theta}^{2}\cos\theta+\dot{\theta}^{2}\dot{\theta}^{2}\cos\theta+\dot{\theta}^{2}\dot{\theta}^{2}\sin^{2}\theta\right)$ = 1 I220 + 2m (R30 + 620 - 2R60 caso) T= 1/Lzz+MR2+ME2/02-REACOSÓ Aside: Q=O...why?

Only potential energy is from the eccentricity, $V = mqh = mq(-\epsilon case)$

So, /=T-V L= I(Izz+mR2+me2) = -mRe= cos+ mqecos0

for 9=0 $\frac{d+\left(\frac{90}{97}\right)-\frac{90}{97}=0}{9}$

 $\frac{\partial \mathcal{L}}{\partial \dot{\Theta}} = \left(\mathbf{I}_{22} + mR^2 + me^2 \right) \dot{\Theta} - 2mRe \dot{\Theta} \cos\Theta \qquad \frac{\partial}{\partial \dot{\Theta}} \left(\frac{\partial \mathcal{L}}{\partial \dot{\Theta}} \right) = \left(\mathbf{I}_{22} + mR^2 + me^2 \right) \dot{\Theta} - 2mRe \dot{\Theta} \cos\Theta + 2mRe \dot{\Theta}^2 \sin\Theta$

If assuming no slip, then

MORK

nether for Nourtual

AG=mREOSINO-MgESINO

(Izz+mR2+M2-2mRecose) = + mRe 62 sin 0 + mqesin 0 = 0