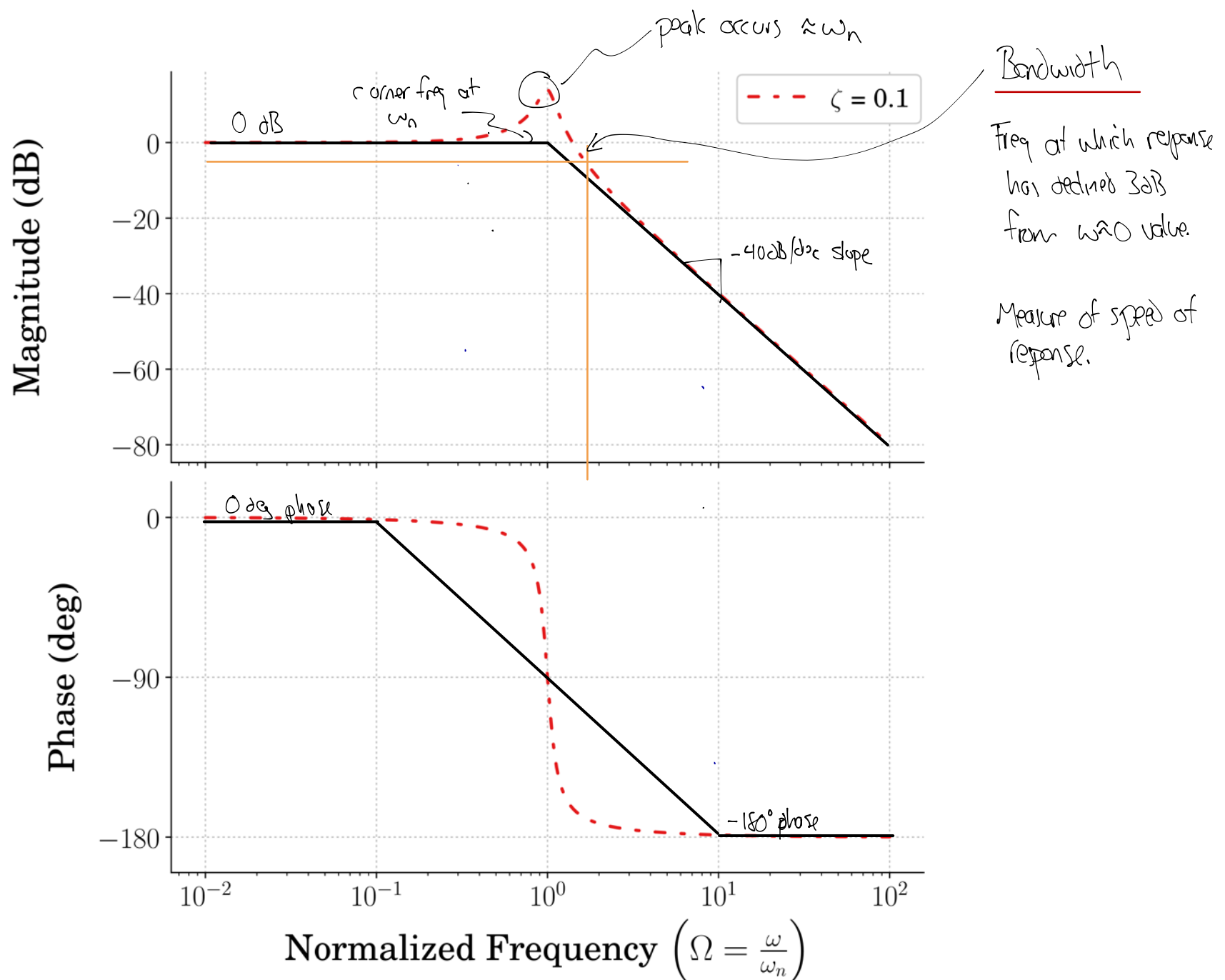
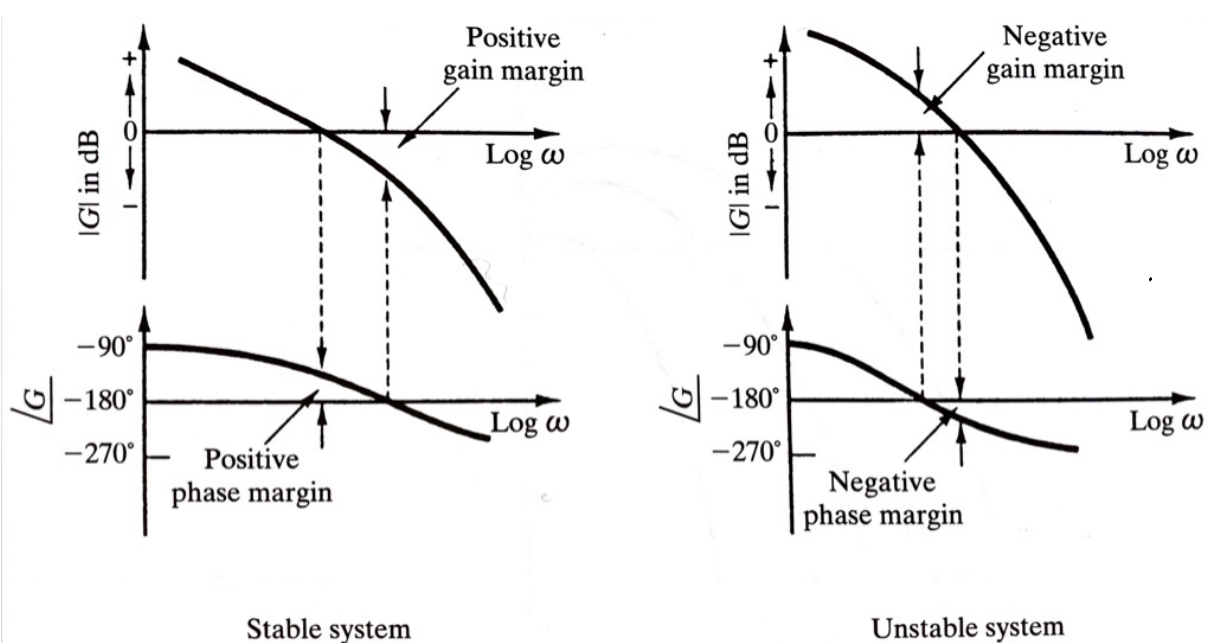


System Performance Analysis with Bode Plots



Gain Margin Amount below 0dB when phase crosses -180deg

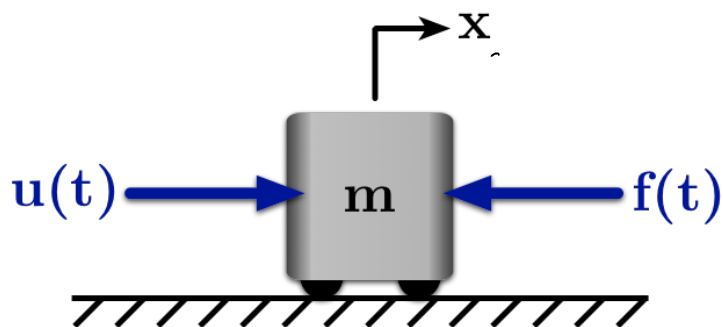
Phase Margin Amount above -180deg when gain crosses 0dB



Gain margin also shows how much gain can change before becoming stable/unstable (How much to increase if stable or how much to decrease if unstable)

From the 1st Day of Class

Let's look again at the model



Found $m\ddot{x} = u - f$

For our PD controller

$$u(t) = k_p(x_d - x) + k_d(\dot{x}_d - \dot{x})$$

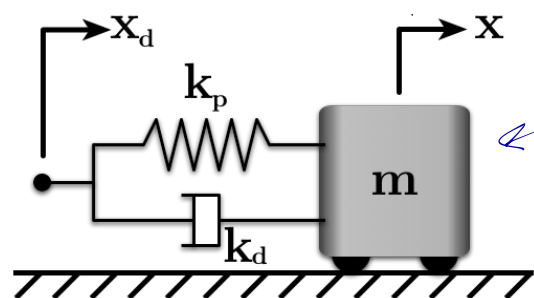
If $f(t) = 0$

$$m\ddot{x} = k_p(x_d - x) + k_d(\dot{x}_d - \dot{x})$$

Q: Does that equation look familiar?

Q: What mechanical element produces force prop. to a difference in position? \leftarrow linear spring

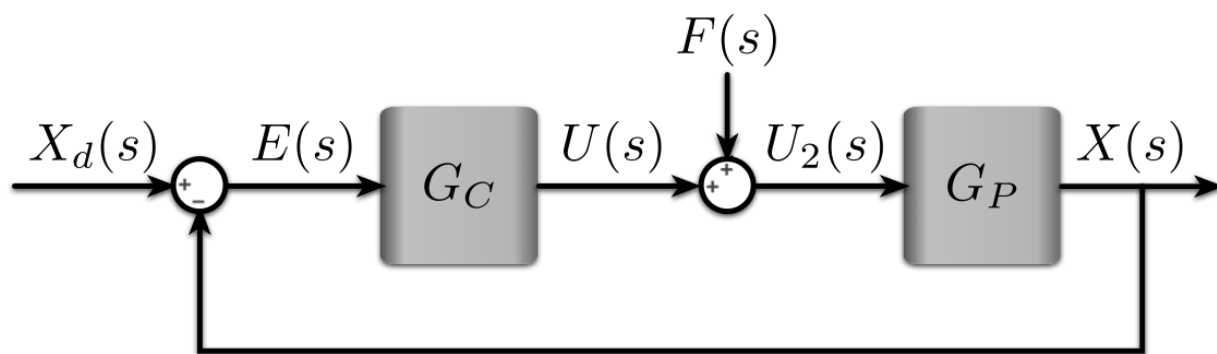
Q: What mechanical element produces force prop. to the rate of change of its length? \leftarrow viscous damper



\leftarrow Our PD controller is mathematically equivalent to this system!!!

Intuitively, you can think of a PD controller acting as a virtual spring-damper between the current state of the system and the desired state.

Q: What is the block diagram of this system?



Q: What is the TF from X_d to X , with $f(t) = 0$

$$m\ddot{x} + k_d\dot{x} + k_p x = k_d\dot{x}_d + k_p x \rightarrow (ms^2 + k_d s + k_p)X(s) = (k_d s + k_p)X_d(s)$$

$$\frac{X}{X_d} = \frac{k_d s + k_p}{ms^2 + k_d s + k_p} \rightarrow \text{divide by } m = \frac{2\zeta\omega_n s + \omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2} \quad 2\zeta\omega_n = \frac{k_d}{m} \quad \omega_n^2 = \frac{k_p}{m}$$

Q: What is the TF from F to X with $x_d(t)=0$

$$m\ddot{x} = k_p(\overset{0}{\cancel{x_d}} - x) + k_d(\overset{0}{\cancel{\dot{x_d}}} - \dot{x}) - f$$

$$m\ddot{x} + k_d\dot{x} + k_p x = f \rightarrow (ms^2 + k_d s + k_p)\bar{X} = F$$

$$\frac{X}{F} = \frac{1}{ms^2 + k_d s + k_p} \rightarrow \text{divide by } m \rightarrow \frac{X}{F} = \frac{1/m}{s^2 + 2\zeta\omega_n s + \omega_n^2} \quad \begin{aligned} 2\zeta\omega_n &= \frac{k_d}{m} \\ \omega_n^2 &= \frac{k_p}{m} \end{aligned}$$

Q: If we want $X=0$ for all time ($x_d(t)=0$) how should we select k_p and k_d ?
steady state

$$\lim_{t \rightarrow \infty} x(t) = \lim_{s \rightarrow 0} sX(s)$$

Look at step input in $f(t)$, $F(s) = \frac{1}{s}$

$$= \lim_{s \rightarrow 0} s \left[\frac{1}{ms^2 + k_d s + k_p} \left(\frac{1}{\cancel{s}} \right) \right] = \lim_{s \rightarrow 0} \frac{1}{ms^2 + k_d s + k_p} = \frac{1}{k_p} \leftarrow \text{we need a large } k_p$$

Q: Can x_{ss} ever be zero for this case?

No $k_p \rightarrow \infty$ for that to happen

Q: How can we select gains $k_p + k_d$?

1) It's a 2nd order system, so we can work directly from the perf measures

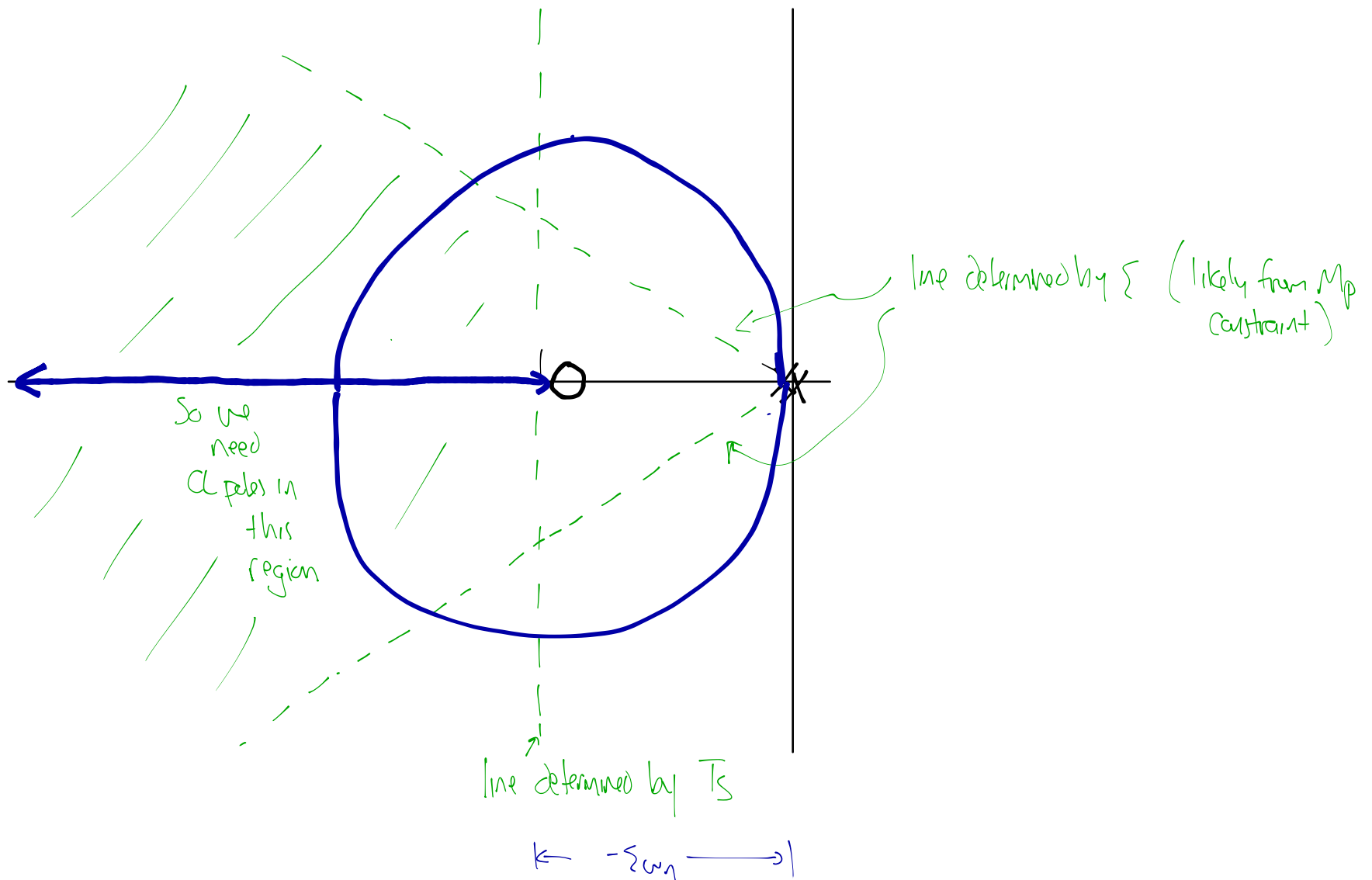
$$M_p = 100\% \times \exp\left[\frac{-\zeta\pi}{\sqrt{1-\zeta^2}}\right]$$

$$T_p = \frac{\pi}{\omega_d}$$

$$T_s = \frac{4}{\zeta\omega_n}$$

\vdots

} These also map out regions on the root locus



The CL TF for this system

$$G_c G_p = (k_d s + k_p) \left(\frac{1}{m s^2} \right) = \frac{k_d s + k_p}{m s^2} \rightarrow$$

$$\frac{k_p \left(\frac{k_d}{k_p} s + 1 \right)}{m s^2}$$

fix this ratio to start

zero at $-\frac{k_p}{k_d}$

Double pole at 0

Asymptotes:

$$\sigma_A = \frac{\sum p_i - \sum z_i}{n-m} = \frac{0 - \frac{k_p}{k_d}}{2-1} = -\frac{k_p}{k_d}$$

$$\phi_A = \left(\frac{2k+1}{n-m} \right) 180^\circ \quad k=0 \rightarrow \phi_A = 180^\circ$$

Q: What can we say about the freq. resp on this system?

Sketch the Bode Plot of closed-loop system

$$\frac{X}{X_d} = \frac{2\zeta\omega_n s + \omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

$$2\zeta\omega_n = \frac{k_d}{m} \quad \omega_n^2 = \frac{k_p}{m}$$

zero at $\frac{-\omega_n}{2\zeta} \rightarrow$ use $\rightarrow 10$ here

complex conjugate poles $\rightarrow \omega_n$

