MCHE 474: Control Systems

Fall 2017 – Mid-Term 2

Thursday, November 9

Name:	Answer Key	CLID:

Directions: Complete the attached problems making sure to clearly indicate your answer, show your work, and list any assumptions that you have made (with justification for them, if necessary). If you need extra space for any question, you may attach additional sheets of paper, which will be provided to you. No calculators are allowed.

Academic Honesty (just a reminder):

An essential rule in every class of the University is that all work for which a student will receive a grade or credit be entirely his or her own or be properly documented to indicate sources. When a student does not follow this rule, s/he is dishonest and s/he defeats the purpose of the course and undermines the goals of the University.

Problem 1 – 40 Points

For the block diagram shown in Figure 1:

- a. Write the closed-loop transfer function.
- b. Write the closed-loop natural frequency in term of K and K_1 .
- c. Write the closed-loop damping ratio in term of K and K_1 .
- d. Assuming J = 1 kg-m², find values of K and K_1 that would result in a maximum percent overshoot of 25% and a peak time of 2s.

Note: Just set up the equations needed to calculate the actual numerical values. Do so in a way such that all that would remain is plugging them into a calculator for solution.

- e. What is the setting time for that choice of K and K_1 ?
- f. What is the steady-state response of y(t) to a unit step input in r(t)?

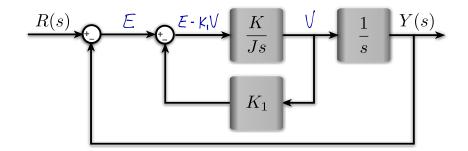
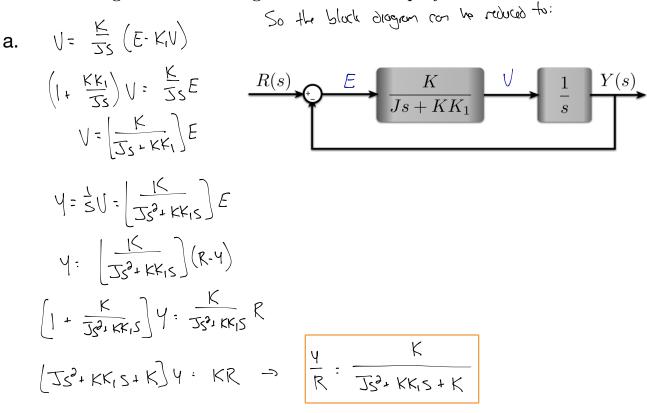


Figure 1: Block Diagram for Closed-loop System



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Problem 1 (cont.)

b.

$$\mathcal{M}_{S}^{U} = \frac{2}{k^{2}} \xrightarrow{R} \mathcal{M}^{2} \xrightarrow{R} \xrightarrow{R} \mathcal{M}^{2} \xrightarrow{R} \mathcal{M}^$$

c.
$$\Im(m) = \frac{2}{Kk^{1}} \rightarrow \xi = \frac{3m^{2}}{Kk^{1}} = \frac{32k^{2}}{Kk^{1}}$$

d. To oversheat = 100 exp
$$\left(\frac{-\xi\pi}{(1-\xi^2)}\right) = 25^{\circ}$$

 $exp\left(\frac{-\xi\pi}{(1-\xi^2)}\right) = 0.25$
 $\frac{-7\pi}{(1-\xi^2)} = \ln(0.25) \qquad \text{plug in solver to find } \xi = 0.404$). Not necessary
is necessary to 25% oversheat) exam
is necessary to 25% oversheat) exam
Peak thue $T_p = \frac{\pi}{2} = \frac{\pi}{60^{\circ}/5} = 25$
need $\omega d = \frac{\pi}{2} \cdot \frac{60^{\circ}}{5} = -5$ $\omega_n = \frac{\omega d}{(1-\xi^2)} \leftarrow plug \text{ in } \xi \text{ four above}$
Then, set $\omega_n - \sqrt{\frac{K}{5}} \cdot \sqrt{K} = 1.72 \frac{60}{5}$

So,
$$K = 2.95$$

We then use $k_1 = \frac{25\omega_n Z}{K}$ to find $k_1 = 0.47$ Provenical values not necessary on the example

e. The settling time is

$$T_s = \frac{4}{\epsilon \omega_n}$$
 so, using the 5 and ω_n from part d., we find
 $T_s = \frac{4}{(0.4 \text{ orb}(1.72))} = 5.76\text{ s}$ numerical value not necessary on the exam

Problem 1 (cont.)

f. We found the CLTF to be:

$$\frac{Y}{R} := \frac{K}{JS^{2} + KK_{1}S + K} \qquad So \qquad Y = \left[\frac{K}{JS^{2} + KK_{1}S + K}\right]R$$
For a skp input $R(S) = \frac{A}{S}$ where A is the skep amplitude.
To find the steady state value, uso the final value Theorem:

$$\lim_{k \to \infty} Y(L) := \lim_{S \to 0} S \left[\left(\frac{K}{JS^{2} + KK_{1}S + K}\right) \right]^{k} := \lim_{S \to 0} \frac{KA}{JS^{2} + KK_{1}S + K}$$

$$\lim_{S \to 0} SY(L) := A$$

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Problem 2 – 40 Points

Consider a system represented by the block diagram in Figure 2, where:

$$G(s) = \frac{K}{s^2(s+1)}$$
 and $H(s) = 1$

- a. Sketch the root locus for this system.
- b. Is this system stable for any nonzero value of K? Why or why not? (*Hint:* Use the root locus you just drew to support your answer.

Now, add a zero to the transfer function of G(s), such that

$$G(s) = \frac{K(s+a)}{s^2(s+1)}$$
 and $H(s) = 1$

where $0 \leq a < 1$.

- d. Sketch the root locus for this new system.
- e. Is this system *unstable* for any nonzero value of K? Why or why not? (*Hint:* Use the root locus you just drew to support your answer.
- f. What is the steady-state error of this system in response to a ramp input?
- g. Without calculating it directly, do you expect this system to have a nonzero, but finite steady-state error in response to a parabolic input? Why or why not?

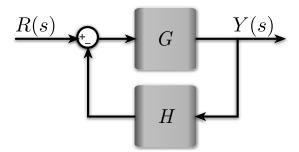
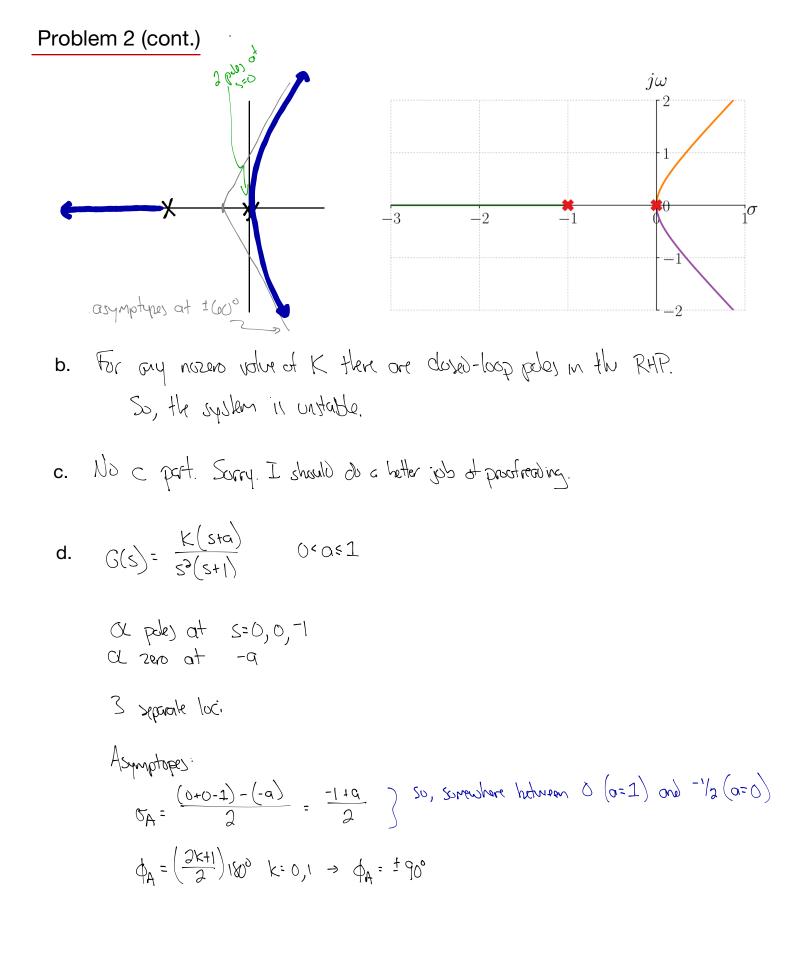


Figure 2: A Unity Feedback System

a. OL poly at
$$s=0,0,-1$$

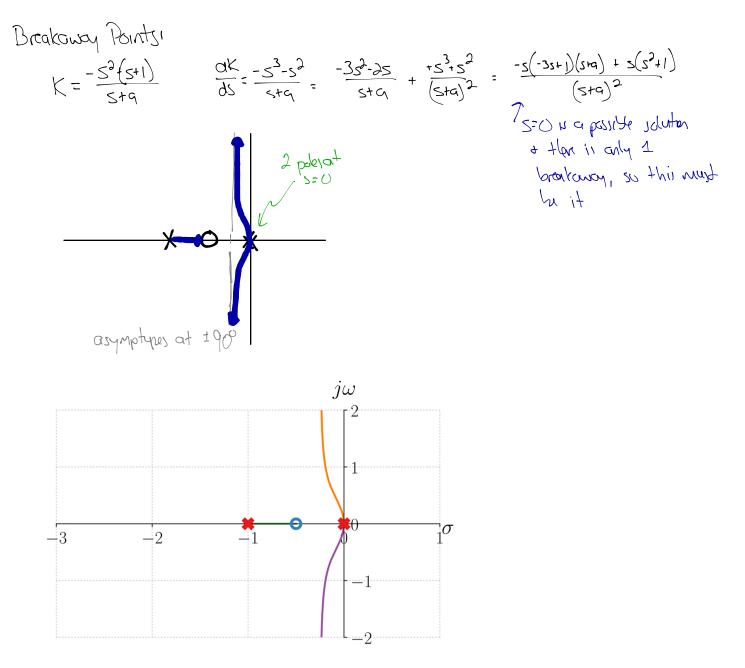
There will be 3 speak luci
 $\sigma_{A} = \frac{z_{PJ} - z_{Zi}}{n-m} = \frac{(0+0-1)}{3}$
 $\varphi_{A} = \left(\frac{2k+1}{n-m}\right) 160^{\circ} \quad k=0,1,2 = \left(\frac{2k+1}{3}\right) 160^{\circ} \quad k=0,1,2 \rightarrow \pm 60^{\circ}, 160^{\circ}$
breakdowey $\rightarrow at = where \frac{\partial k}{\partial s} = 0$
 $k=-s^{2}(s+1):-s^{3} \cdot s^{2} \quad \frac{\partial k}{\partial s} :-3s^{2} \cdot 2s:-s(s+\frac{2}{3}) \rightarrow s=0, s:-\frac{2}{3}$
rot on here super supe

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Problem 2 (cont.)



e. The doxo-loop poles for this system are never in the RHP, so it is always stable.

Problem 2 (cont.)

- f. This is a Type 2 system, so its steady-state error to a ramp input in 0. If you didn't remarker this, we need to. Fus E(s) for the CLTF H=1, 50 ... $\frac{Y(s)}{1 + G} = \frac{1}{R}$ E= R-Y= R-GE GH $G = \frac{K(s+a)}{s^{2}(s+1)} \quad so \quad \frac{E}{R} = \frac{s^{2}(s+1)}{s^{2}(s+1) + K(s+a)} \quad E = \frac{s^{2}(s+1)}{s^{2}(s+1) + K(s+a)} R$ R(s)= 5= for a unit ramp input so $E(s) = \frac{s^{2}(s+1)}{s^{2}(s+1) + K(s+q)} \left(\frac{1}{s^{2}}\right)$ $\lim_{t \to \infty} e(t) = \lim_{s \to 0} sE(s) = \frac{s(s+1)}{s^2(s+1) + k(s+\alpha)} = \bigcirc$
- g. This is a Type 2 system, so it will have a finite steady-state error in response to a parabolic imputi

$_$ Problem 3 – 20 Points

For the system in the block diagram in Figure 3:

$$G_p(s) = \frac{10}{s(s+1)}$$
 and $G_c(s) = \frac{s+a}{s+8}$

where a is a positive constant.

- a. What is the open-loop transfer function this system?
- b. What is the closed-loop transfer function this system?
- c. Sketch the root locus for this system for variation in parameter a.

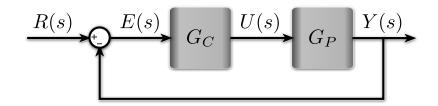


Figure 3: Block Diagram of a Feedback Control System

a.
$$O(TF: GCp = \frac{10(Sta)}{S(St1)(St8)})$$

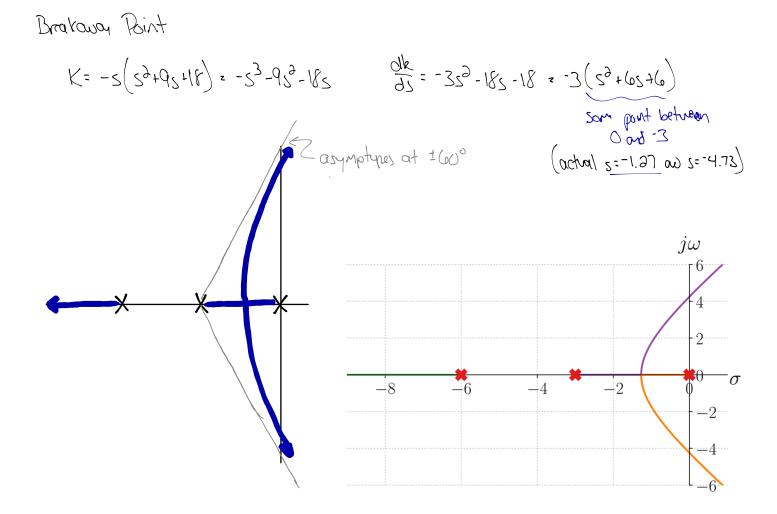
b. $CLTF: \frac{GCp}{1+(sCp)} = \frac{10(Sta)}{S(St1)(St8) + 10(Sta)}$
c. In its connect form, a is not in the connect "place" for Stabeling o reat
locus based on its Usuation. So, we need to rearpulate the char of so
that it is. The current char eq. is
 $S(St1)(St8) + 10(Sta) = 0$
Divide by all terms except 109
 $\frac{S(St1)(St8) + 10S + 109}{S(St1)(St8) + 10S + 105} = 0 \rightarrow 1 + \frac{109}{S(St1)(St8) + 10S} = 0$
 $\rightarrow 1 + \frac{109}{S(St^2 + 9S + 18)} = 0$
Now, this is mic tare we
converted a not locus

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Problem 3 (cont.)

$$1 + \frac{109}{5(5^{2}+95+18)} = 0$$
 Define K= 109

$$\sigma_{A} = \frac{0.3.6}{3} = -3 \qquad \qquad \varphi_{A} = \left(\frac{3^{k+1}}{3}\right)^{1} 80^{\circ} \quad k = 0, 1, 2 \rightarrow \varphi_{A} = \pm 60^{\circ}, 180^{\circ}$$



Possibly Useful Equations

$$\bar{f} = m\bar{a}$$

$$I_0\bar{\alpha} = \sum \bar{M}_0$$

$$\sin(a \pm b) = \sin(a)\cos(b) \pm \cos(a)\sin(b)$$

$$\cos(a \pm b) = \cos(a)\cos(b) \mp \sin(a)\sin(b)$$

$$e^{\pm i\omega t} = \cos(\omega t) \pm i\sin(\omega t)$$

$$x(t) = ae^{i\omega_n t} + be^{-i\omega_n t}$$

$$x(t) = a\cos\omega_n t + b\sin\omega_n t$$

$$x(t) = e^{-\zeta\omega_n t} [a\cos(\omega_d t) + b\sin(\omega_d t)]$$

$$x = \frac{-b \pm \sqrt{b^2 - 4ac}}{2a}$$

$$\int u \, dv = uv - \int v \, du$$

$$\delta_{oc} V = \forall \sum$$

$$\begin{split} \dot{\mathbf{x}} &= A\mathbf{x} + B\mathbf{u} \\ \mathbf{y} &= C\mathbf{x} + D\mathbf{u} \end{split}$$
$$\mathbf{x} &= \mathbf{\Phi}(t)\mathbf{x}(0) + \int_{0}^{t} \mathbf{\Phi}(t-\tau)\mathbf{B}\mathbf{u}(\tau)d\tau \\ \mathbf{X}(s) &= [s\mathbf{I} - \mathbf{A}]^{-1}\mathbf{x}(0) + [s\mathbf{I} - \mathbf{A}]^{-1}\mathbf{B}\mathbf{U}(s) \\ S_{\alpha}^{T} &= S_{G}^{T}S_{\alpha}^{G} \\ T_{s} &= \frac{4}{\zeta\omega_{n}} \\ T_{r} &\approx \frac{2.16\zeta + 0.60}{\omega_{n}}, \quad 0.3 \leq \zeta \leq 0.8 \\ T_{p} &= \frac{\pi}{\omega_{n}\sqrt{1-\zeta^{2}}} \\ M_{P_{t}} &= 1 + e^{-\zeta\pi/\sqrt{1-\zeta^{2}}} \\ M_{P_{t}} &= 1 + e^{-\zeta\pi/\sqrt{1-\zeta^{2}}} \\ \nabla(0 \text{vershoot} &= 100e^{-\zeta\pi/\sqrt{1-\zeta^{2}}} \\ V(\omega, \zeta) &= e^{-\zeta\omega t_{n}}\sqrt{[C(\omega, \zeta)]^{2} + [S(\omega, \zeta)]^{2}} \end{split}$$

Table 1: Laplace Transform Pairs

f(t)	F(s)
$f(t) = A, \forall t > 0$	$\frac{A}{s}$
$f(t) = At, \forall t > 0$	$\frac{A}{s}$ $\frac{A}{s^2}$
$\delta(t)$	1
e^{-at}	$\frac{1}{s+a}$
$\sin \omega t$	$\frac{\omega}{s+\omega^2}$
$\cos \omega t$	$\frac{s}{s+\omega^2}$
$e^{-at}\sin\omega t$	$\frac{\omega}{(s+a)^2+\omega^2}$
$e^{-at}\cos\omega t$	$\frac{s+a}{(s+a)^2+\omega^2}$
$\frac{\omega_n}{\sqrt{1-\zeta^2}}e^{-\zeta\omega_n t}\sin\left(\omega_n\sqrt{1-\zeta^2}\right),\zeta<1$	$\frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$
$\frac{\omega_n}{\sqrt{1-\zeta^2}} e^{-\zeta\omega_n t} \sin\left(\omega_n \sqrt{1-\zeta^2}\right), \zeta < 1$ $1 - \frac{1}{\sqrt{1-\zeta^2}} e^{-\zeta\omega_n t} \sin\left(\omega_n \sqrt{1-\zeta^2} + \phi\right), \phi = \cos^{-1}\zeta, \zeta < 1$	$\frac{\omega_n^2}{s(s^2+2\zeta\omega_ns+\omega_n^2)}$

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