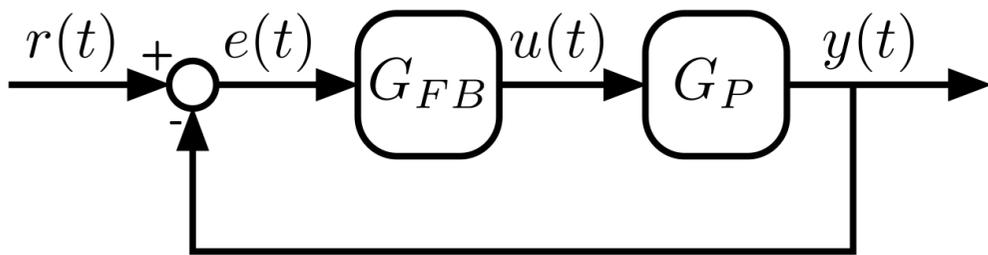
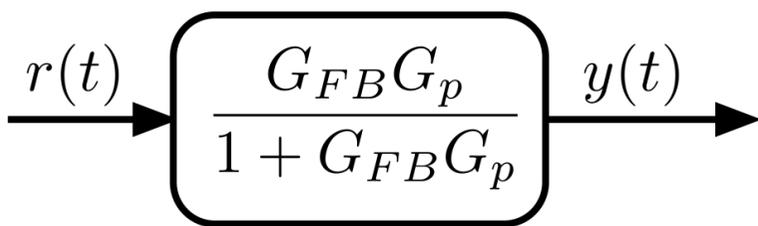


# Tracking Control

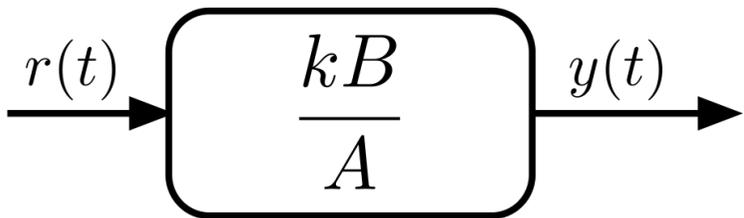


Q: What should  $r(t)$  be such that  $y(t) = y_d(t)$ ?

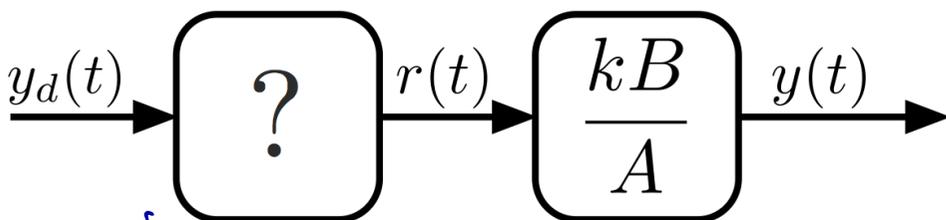
Let's simplify the block diagram to investigate



or generically

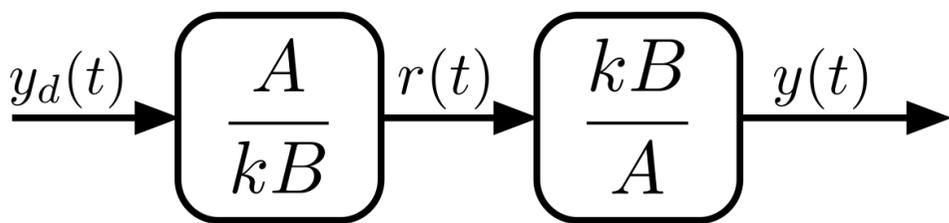


Q: So, what should  $r(t)$  be?



What should this be?

Let's try the inverse of the system.

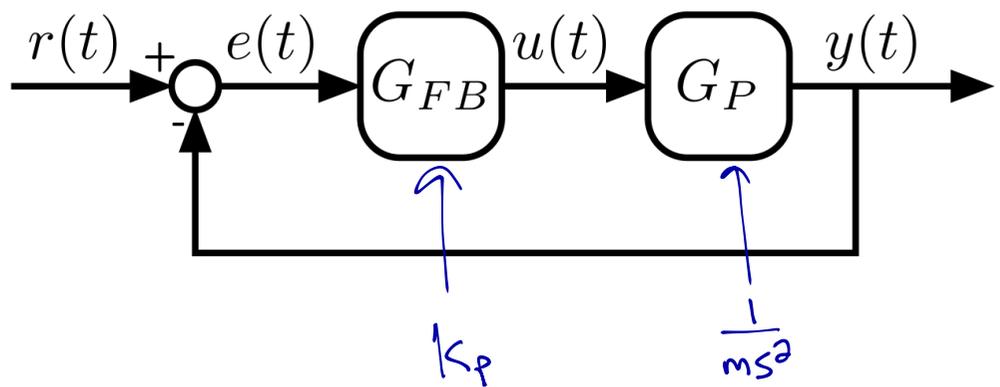
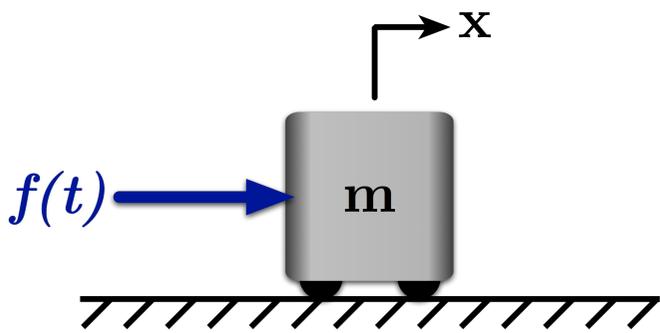


Plant Inversion

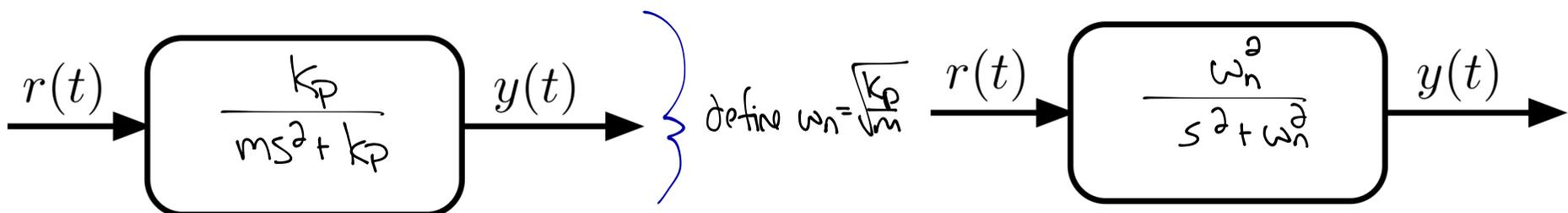
$$\begin{aligned} r(t) &= \frac{A}{kB} y_d(t) \\ y(t) &= \frac{kB}{A} r(t) = \frac{kB}{A} \left[ \frac{A}{kB} y_d(t) \right] \\ &= y_d(t) \end{aligned}$$

# Plant Inversion Example

system is just a mass under prop. control.



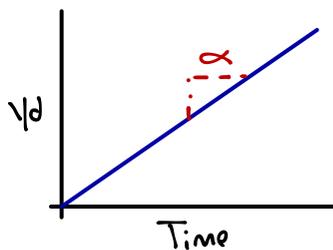
In simplified form:



So, for this system  $k_B = \omega_n^2$  and  $A = s^2 + \omega_n^2$

Let's try to track a ramp:

$$y_d(t) = \alpha t$$



In the Laplace domain

$$y_d(s) = \frac{\alpha}{s^2}$$

$$r(t) = \frac{A}{k_B} y_d(t)$$

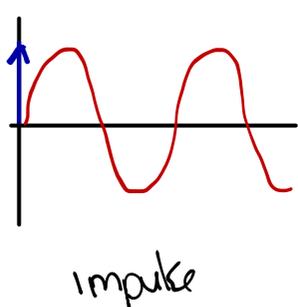
$$r(s) = \frac{A}{k_B} y_d(s) = \left( \frac{s^2 + \omega_n^2}{\omega_n^2} \right) \left( \frac{\alpha}{s^2} \right)$$

$$= \alpha \left( \frac{s^2 + \omega_n^2}{s^2 \omega_n^2} \right) = \frac{\alpha}{s^2 \omega_n^2} \left( 1 + \frac{\omega_n^2}{s^2} \right)$$

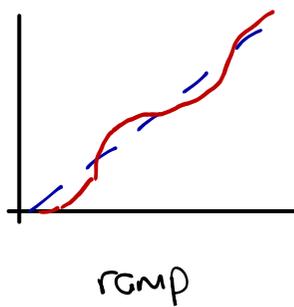
Converting back to time domain

via inverse Laplace Trans.

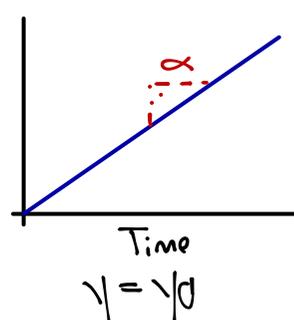
$$r(t) = \frac{\alpha}{\omega_n^2} \left( \underbrace{f(t)}_{\text{impulse}} + \underbrace{\omega_n^2 t}_{\text{ramp}} \right)$$



+



=



# Plant Inversion Example (cont.)

Q: What's the problem with this?

Look at the force this  $r(t)$  generates:

$$y(s) = \frac{f(s)}{ms^2} \rightarrow f(s) = ms^2 y(s) = ms^2 \left( \frac{\omega}{s^2} \right)$$

$$f(s) = m\omega \rightarrow \text{convert to time domain} \rightarrow f(t) = m\omega f(t)$$

This is a problem!

We cannot generate an  $\infty$  force

Q: What other problems are there?

We've assumed our model exactly matches the "real" system...

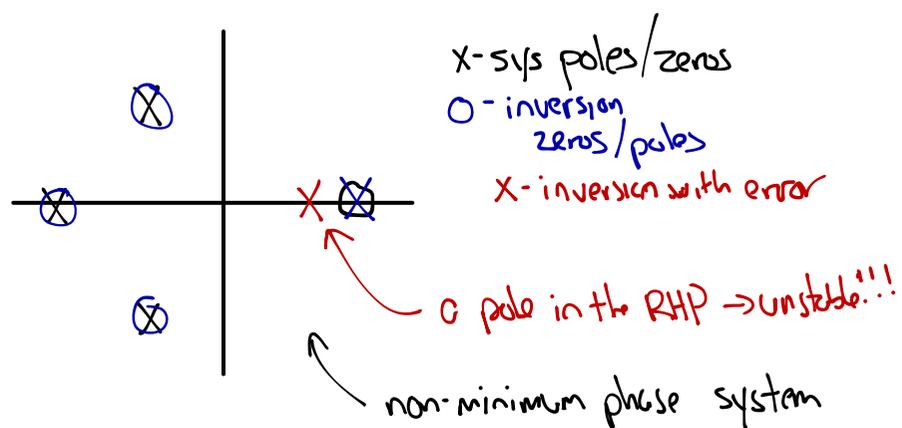
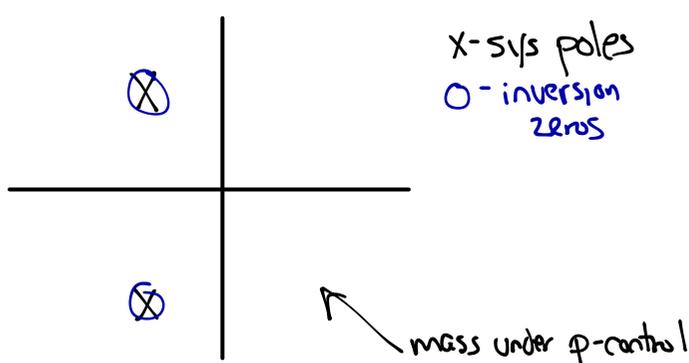
But, it never exactly matches. So, we don't get the nice cancellation

## Limitations of Plant Inversion:

- Desired states must be achievable
- Model must be \*very\* good
- Closed loop transfer function must be in the \*right\* form

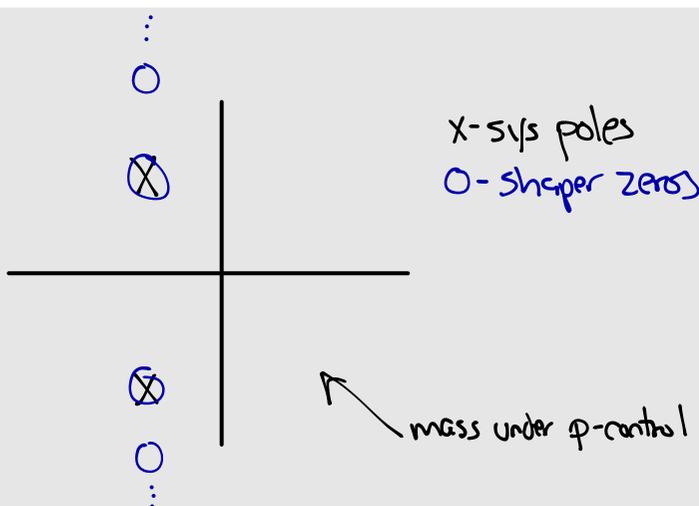
What is the right form?  
(or wrong)

To answer, let's look at this method in the s-plane



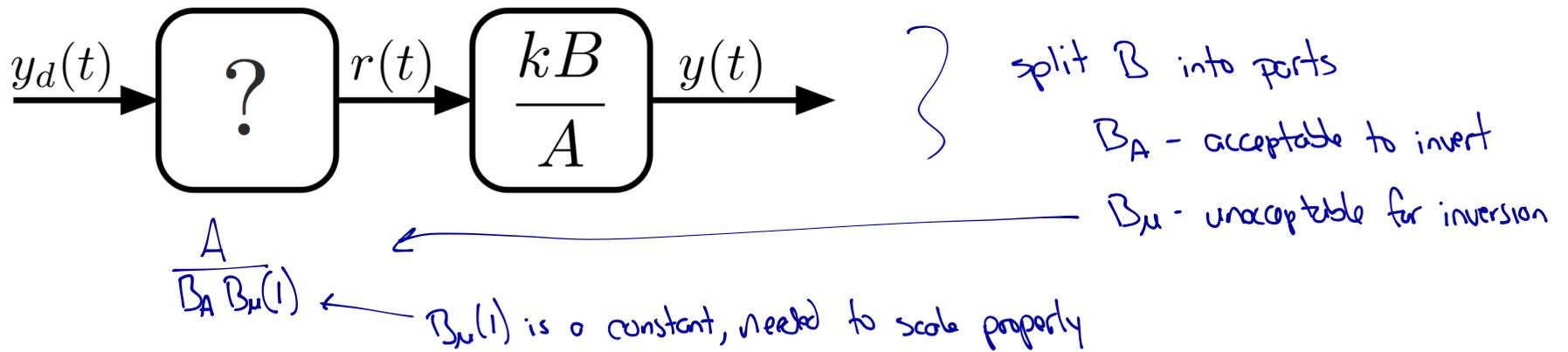
Aside:

Input shaping places a column of zeros over flexible poles.



# Zero Phase Error Tracking Controller (ZEPTC)

The problem with inversion is RHP zeros, so just don't invert those



$$\begin{aligned}
 \text{So, } Y &= \begin{bmatrix} A \\ B_A B_u(s) \end{bmatrix} \begin{bmatrix} kB \\ A \end{bmatrix} Y_d \\
 &= \begin{bmatrix} A \\ B_A B_u(s) \end{bmatrix} \begin{bmatrix} B_A B_u \\ A \end{bmatrix} Y_d \\
 Y &= \frac{B_u}{B_u(s)} Y_d
 \end{aligned}$$

you can think of ZPETC as "partial" model inversion

Note: There are a few more steps for a "real" ZPETC. Below is the final form, It is usually shown in the digital domain.

$$r(k) = \frac{A(z^{-1}) B_u(z^{-1})}{B_A(z^{-1}) [B_u(s)]^d} Y_d(k+dTs)$$

$d$  = time delay inherent to plant  
 $s$  = # of unacceptable zeros

See slides for example.

# Repetitive Learning Control

Repeated Trajectories are common in:

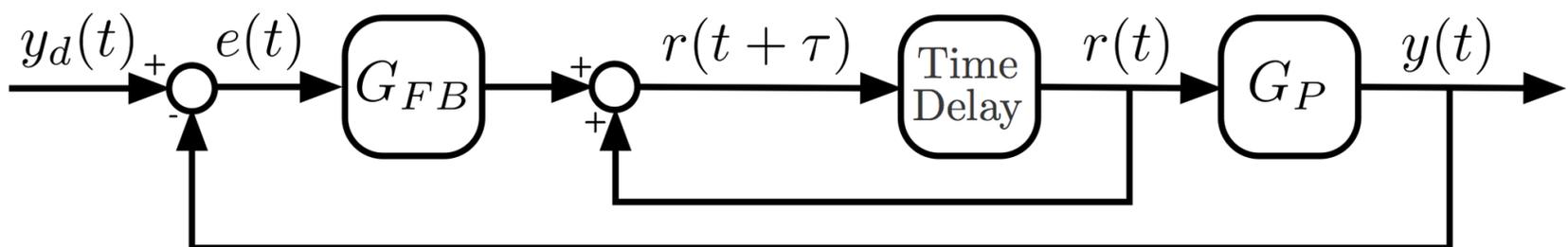
- manufacturing
- machining
- robotics
- scanning
- automated cranes (the few that are existence)

Objective: "Learn" a good control input while tracking a repeated (periodic) trajectory

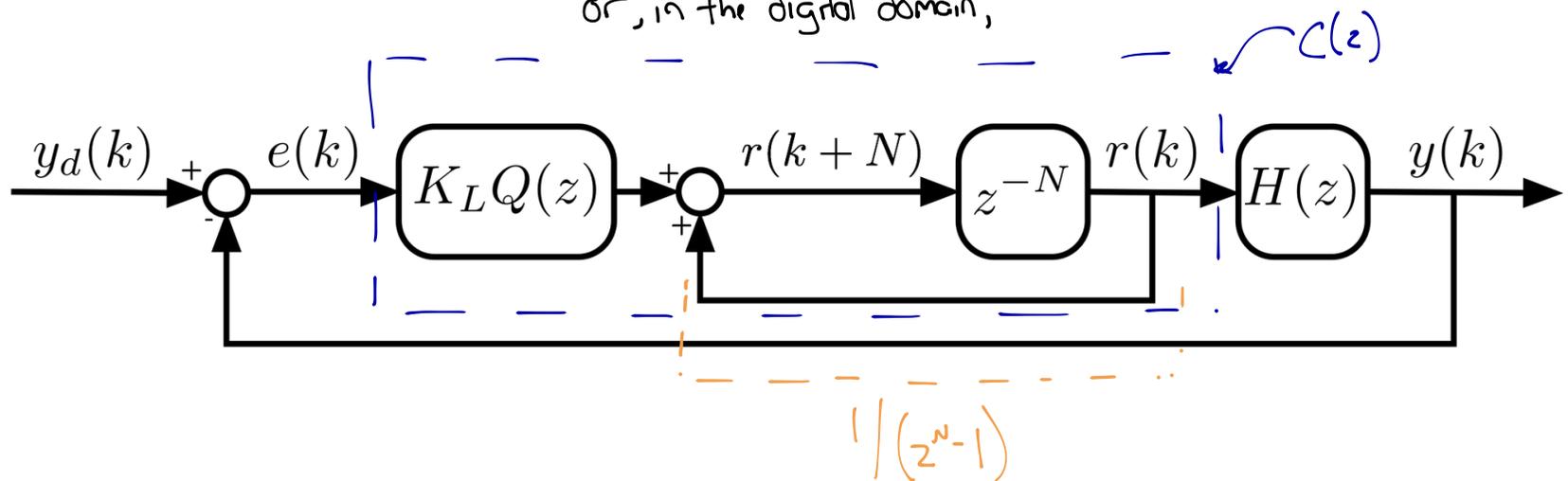
Q: What is a repeated trajectory, mathematically?

$$y_d(t+\tau) = y_d(t) \quad \text{or} \quad y_d(k) = y_d(k+N)$$

↑ periodic of traj.
↑ # of timesteps in period of traj.



or, in the digital domain,



$$C(z) = \frac{K_L Q(z)}{z^N - 1}$$

$K_L > 0$  - learning gain

$N$  - period of repetition (in # of samples)

$Q(z)$  - "feedback" controller

# Repetitive Learning Control (cont)

Let's look at the reference input  $r(k)$ :

$$r(k+N) = r(k) + K_L Q(z) [y_d(k) - y(k)]$$

input next cycle      input this cycle      compensation for error during this cycle

Q: What's the effect of increasing  $K_L$ ?

- more emphasis on error
- faster "learning"
- BUT more sensitive to noise